# STORMWATER DESIGN NARRATIVE 

PREPARED November 21, 2022

APPLICANT:
HARSH REALTY LLC
248 Atlantic Ave, Hull, MA 02045

PROJECT:

## 248 ATLANTIC AVE

248 Atlantic Ave, Hull, MA 02045

PREPARED BY:
PVI SITE DESIGN, LLC
18 GLENDALE ROAD, NORWOOD, MA 02062


## SECTION 1 - PROJECT OVERVIEW

### 1.1 INTRODUCTION

The applicant, Harsh Realty LLC, is proposing to redevelop the commercial property located at 248 Atlantic Ave, Hull, MA, parcel ID 49-078. This lot is currently developed with a two-story mixeduse building with a coffee shop on the ground floor and residential above. The total lot area is $4,025 \mathrm{sf}$ ( 0.092 acres) and is in the Business zone.

The project proposes to demolish the existing building and replace it with a new building with a similar footprint. The project will result in an increase of impervious area. In accordance with Hull Zoning By-Law section 410-4-l.D.l.g, the project shall address the prevention of pollution of surface and groundwater, soil erosion, increased runoff and flooding. This will be achieved with the implementation of Best Management Practices (BMPs) such as porous pavement and an underground infiltration trench, as further described in this report.

### 1.2 LOCATION, TOPOGRAPHY, AND SOILS

LOCATION:
The project site is located at 248 Atlantic Ave, Hull, MA. The property has frontage on Atlantic Ave. There are no existing curb cuts and no on-site parking. The property sits at the intersection of Atlantic and School Streets, across the street from Town Hall.

## TOPOGRAPHY

The topography within the subject site slopes generally from the southwest to the northeast, or from the front left corner on Atlantic Ave to the back right corner at the abutting property line. Elevations range from 51 feet to 47 feet. Slopes are gentle across the front two-thirds of the site, with the rear of the site reaching slopes of $10 \%$. The proposed design aims to maintain the existing topography.

## SOILS

The underlying soils have been obtained from the Natural Resources Conservation Service as made available by the Web Soil Survey website and are generally consistent across the site. The soil types are as follows:

## TABLE 1.1 - NRCS SOIL TYPES

| NRCS MAP UNIT | MAP UNIT NAME | HYDROLOGIC SOIL GROUP |
| :---: | :---: | :---: |
| 635 | Canton-Urban Land | A |

A copy of the NRCS Web Soil Survey maps is included in the Appendix of this report.

### 1.3 WATERSHED DESCRIPTIONS

The Development Area consists of two watershed areas for the purpose of this stormwater analysis. Below is a discussion of the watersheds. Refer to Figure 2 and Figure 3 for Existing and Proposed Watershed Plans respectively. Watershed plans provide information on total area, Curve Numbers, and Time of Concentration for each watershed.

### 1.3.1 EXISTING CONDITIONS

WATERSHED EX-1

The northern portion of the site drains to the northeast corner where runoff discharges to the abutter's rear yard. Runoff from portions of the building, pavement, and landscape areas, totaling 2,622 sf, contributes to this design point. For the purposes of the analysis, the property line will be considered the Design Point, DP-1.

WATERSHED EX-2
The southern portion of the site drains to the southeast corner where runoff discharges to the gutter line in Atlantic Ave. This watershed also includes portions of the building, pavement, and landscape areas. This watershed is comprised of $1,403 \mathrm{sf}$. For the purposes of the analysis, the property line will be considered the Design Point, DP-2.

### 1.3.2 PROPOSED CONDITIONS

The proposed project includes replacing the existing building with a new building of a similar footprint. As in the existing condition, paved walkways will provide access to the building. The remaining site area will be landscaped.

## WATERSHED PW-1

The proposed site design reduces the size of the watershed discharging to DP-1, thereby reducing stormwater runoff to the abutting property to the northeast. The design reduces the amount of roof area contributing to this watershed and uses porous pavement to further reduce stormwater runoff. This watershed is comprised of $2,138 \mathrm{sf}$. For the purposes of the analysis, the property line will be considered the Design Point, DP-1.

## WATERSHED PW-2

The proposed site design increases the size of the watershed discharging to DP-2, including an increase to impervious area. This watershed is comprised of $1,887 \mathrm{sf}$. The increase of runoff to this design point is mitigated by collecting and infiltrating runoff from paved areas in front of the building. Runoff not collected will discharge to the gutter line in Atlantic Ave. For the purposes of the analysis, the property line will be considered the Design Point, DP-1.

### 1.4 METHODOLOGY

The peak rate of runoff and sizing of retention BMP's was determined using techniques and data found in the following:

1. Urban Hydrology for Small Watersheds - Technical Release 55 by the United States Department of Agriculture Soils Conservation Service, June 1986. Runoff curve numbers and 24 -hour precipitation values were obtained from this reference.
2. HydroCAD® Stormwater Modeling System by HydroCAD Software Solutions LLC, version 10.0. The HydroCAD program was used to generate the runoff hydrographs for the watershed areas, to determine discharge/stage/storage characteristics for the infiltration systems, to perform drainage routing and to combine the results of the runoff hydrographs. This software is based on the Soil Conservation Service (SCS) TR-20 program.

## SECTION 2 - MITIGATION MEASURES - BEST MANAGEMENT PRACTICES

Best Management Practices were selected as appropriate to provide a drainage system compliant with the Hull Zoning Code.

### 2.1 PEAK RATE ATTENUATION

The proposed system has been designed to mitigate increase in runoff leaving the property due to increased impervious areas. The following table summarizes the results of the calculations:

TABLE 2 - RUNOFF FLOW COMPARISON

| Design Point |  | $\mathbf{2 - Y E A R}$ | 10-YEAR | 100-YEAR |
| :--- | :--- | :---: | :---: | :---: |
| DP-1 | Existing | 0.07 | 0.16 | 0.39 |
|  | Proposed | $\mathbf{0 . 0 6}$ | $\mathbf{0 . 1 3}$ | $\mathbf{0 . 3 2}$ |
| DP-2 | Existing | 010 | 0.15 | 0.28 |
|  | Proposed | $\mathbf{0 . 1 0}$ | $\mathbf{0 . 1 5}$ | $\mathbf{0 . 2 6}$ |

Detailed HydroCAD calculations are provided in the appendix.

### 2.2 ANNUAL RECHARGE TO GROUNDWATER

Annual recharge is based on soil type for the project. As previously noted, the soil type falls within Hydrologic Soil Group A. Following the standard set by MassDEP, for this soil type a recharge rate of 0.60 -inch $x$ the Total Impervious Area. The Required Recharge Volume (RRv) for the increase in impervious area for the property is as follows:

$$
R R v=296 \text { SF } \times 0.60 / 12=15 \text { Cubic Feet }
$$

The infiltration trench has been designed to hold and infiltrate a static volume, below the lowest outlet, of 242 cf, far exceeding the 15 cf required.

## SECTION 3 - OPERATION \& MAINTENANCE PLAN

All stormwater BMPs require on-going maintenance. The following is a brief description for recommended maintenance for the BMP's outlined in this report:

Downspouts:
Building downspouts should be inspected annually towards the end of the fall season to ensure not leaf or other debris has collected and limits flow. Both the top of the downspout, and the connection to the underground pipes should be inspected. Any debris should be removed.

## Permeable Pavers:

Inspection: Inspect parking area after precipitation events at a minimum of four times per year to ensure proper drainage. Inspection should preferably occur during extended precipitation events, high-intensity rainfall, and/or rain-on-snow events. If standing water remains on surface of pavers more than 30 minutes after rainfall has ended, cleaning of porous pavers is recommended.

Cleaning: In Clogged areas power wash aggregate between joints to a minimum of 1 " below paver surface. Refill joints with clean ASTM NO. 8 aggregate material.

Winter Maintenance: Salting of the permeable pavers is permitted. No winter sanding shall be allowed on the permeable paver area, as sand will clog the porous pavement surface. To prevent aesthetic damage to the paver surface (e.g. scarring), shovel area by hand (not with snowblower).

## Underground Infiltration Trenches:

During first year visually inspect after each major storm (>1.5") and again 72 hours later to verify exfiltration is occurring as designed. Note if water remains in basin after 72 hours. After first year visually inspect twice per year. Infiltration Systems shall be inspected for accumulation of silt, sediment, standing water, or debris on an annual basis. Debris and sediment shall be removed.

The inspection port is a 6" PVC riser. Removing the inspection port cover will provide access to the Chamber below. From the surface, through this access, the sediment depth may be measured. A stadia rod may be used to measure the depth of sediment. If the depth of sediment is in excess of 3 inches, then this row should be cleaned with high pressure water through a culvert cleaning nozzle. This would be carried out through an upstream structure. CCTV inspection of this row can be deployed through this access port to determine if any sediment has accumulated in the inlet row.

## Landscaped Areas:

Landscaped areas shall be inspected and maintained on a regular basis. Areas that may be subject to erosion will be stabilized and reseeded immediately. Inspect soil and repair eroded areas monthly. Re-plant void areas as needed. Remove litter and debris monthly. Remove and replace dead vegetation twice per year in spring and fall. Replace soil media if ponding is witnessed more than 48 hours after rainfall event

For further information about the design of the system and on-going maintenance, contact the Engineer of Record:

PVI Site Design, LLC
Attn: Timothy Power, PE

18 Glendale Road
Norwood, MA 02062
tpower@PVIsitedesign.com
339.206.1030

APPENDIX A
Watershed Plans



## APPENDIX B HydroCAD Calculations

- Existing Conditions
- Proposed Conditions
- Infiltration System Stage-Storage Table


EX-1


EX-2


## Summary for Subcatchment 1S: EX-1

Runoff $=\quad 0.07$ cfs @ 12.14 hrs, Volume= 223 cf , Depth> 1.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= $0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$ NRCC 24-hr C 2-Year Rainfall=3.35"

|  | Area (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 997 | 98 | Roofs, HSG A |  |  |
|  | 455 | 98 | Paved parking, HSG A |  |  |
|  | 1,170 | 39 | >75\% Grass cover, Good, HSG A |  |  |
|  | 2,622 | 72 | Weighted Average |  |  |
|  | 1,170 |  | 44.62\% Pervious Area |  |  |
|  | 1,452 |  | 55.38\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 6.0 |  |  |  |  | Direct Entry |

## Summary for Subcatchment 2S: EX-2

Runoff $=\quad 0.10$ cfs @ 12.13 hrs, Volume $=\quad 326$ cf, Depth> 2.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.35"


## Summary for Subcatchment 1S: EX-1

Runoff $=\quad 0.16$ cfs @ 12.13 hrs, Volume $=\quad 471 \mathrm{cf}$, Depth> 2.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= $0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$ NRCC 24-hr C 10-Year Rainfall=4.95"

|  | Area (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 997 | 98 | Roofs, HSG A |  |  |
|  | 455 | 98 | Paved parking, HSG A |  |  |
|  | 1,170 | 39 | >75\% Grass cover, Good, HSG A |  |  |
|  | 2,622 | 72 | Weighted Average |  |  |
|  | 1,170 |  | 44.62\% Pervious Area |  |  |
|  | 1,452 |  | 55.38\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 6.0 |  |  |  |  | Direct Entry |

## Summary for Subcatchment 2S: EX-2

Runoff $=\quad 0.15$ cfs @ 12.13 hrs, Volume= 510 cf , Depth> 4.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.95"


## Summary for Subcatchment 1S: EX-1

Runoff $=\quad 0.39$ cfs @ 12.13 hrs, Volume $=1,156 \mathrm{cf}$, Depth> 5.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= $0.00-24.00 \mathrm{hrs}, \mathrm{dt}=0.05 \mathrm{hrs}$ NRCC 24-hr C 100-Year Rainfall=8.68"


## Summary for Subcatchment 2S: EX-2

Runoff $=\quad 0.28 \mathrm{cfs} @ 12.13 \mathrm{hrs}$, Volume= 944 cf , Depth> 8.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.68"

|  | Area (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1,096 | 98 | Roofs, HSG A |  |  |
|  | 225 | 98 | Paved parking, HSG A |  |  |
|  | 82 | 39 | >75\% Grass cover, Good, HSG A |  |  |
|  | 1,403 | 95 | Weighted Average |  |  |
|  | 82 |  | 5.84\% Pervious Area |  |  |
|  | 1,321 |  | 94.16\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
| 6.0 |  |  |  |  | Direct Entry |



Leaching Basin
DP2


## Summary for Subcatchment 1S: PR-1

Runoff $=\quad 0.06 \mathrm{cfs} @ 12.14 \mathrm{hrs}$, Volume= 182 cf , Depth> 1.02"

Routed to Reach 1R : DP1
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.35"

|  | Area (sf) | CN | Description |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1,044 | 98 | Roofs, HSG A |  |  |
|  | 168 | 98 | Paved parking, HSG A |  |  |
|  | 738 | 39 | >75\% Permeable Pavers, Good, HSG A |  |  |
|  | 188 | 39 | >75\% Grass cover, Good, HSG A |  |  |
|  | 2,138 | 72 | Weighted Average |  |  |
|  | 926 |  | 43.31\% Pervious Area |  |  |
|  | 1,212 |  | 56.69\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \end{array}$ | Length (feet) | Slope $(\mathrm{ft} / \mathrm{ft})$ | Velocity (ft/sec) | $\begin{array}{r} \text { Capacity } \\ (\mathrm{cfs}) \end{array}$ | Description |
| 6.0 |  |  |  |  | Direct Entry, As |

## Summary for Subcatchment 2Sa: PR-2

Runoff $=\quad 0.10$ cfs @ 12.13 hrs, Volume= 329 cf , Depth> 3.00"
Routed to Reach 2R : DP2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 2-Year Rainfall=3.35"


| Area (sf) |  | CN Description |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & 98 \\ & 98 \end{aligned}$ | Paved parking, HSG A Patio, HSG A |  |  |
|  | $\begin{aligned} & 571 \\ & 571 \end{aligned}$ | 98 | eighted A 00.00\% Im | verage pervious A |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \end{array}$ | Length (feet) | Slope <br> (ft/ft) | Velocity (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \end{array}$ | Description |
| 6.0 |  |  |  |  | Direct Entry |


| low Area | 2,138 | 56.69\% Impervious, | Depth > 1.02" for 2-Year event |
| :---: | :---: | :---: | :---: |
| Inflow | 0.06 cfs @ | 12.14 hrs , Volume= | 182 cf |
| Outflow | 0.06 cfs @ | 12.14 hrs , Volume= | 182 cf, Atten= 0\%, Lag= 0.0 |

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Reach 2R: DP2

| Inflow Area |  | 1,316 sf, $97.87 \%$ Impervious, | Inflow Depth $>3.00 "$ | for $2-$ Year event |
| :--- | :--- | :--- | :--- | :--- |
| Inflow | $=$ | $0.10 \mathrm{cfs} @$ | 12.13 hrs , Volume= | 329 cf |
| Outflow | $=$ | $0.10 \mathrm{cfs} @$ | 12.13 hrs , Volume $=$ | 329 cf , Atten $=0 \%$, Lag $=0.0 \mathrm{~min}$ |

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Pond 2P: Leaching Basin



Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev=45.13' @ 12.81 hrs Surf.Area= 90 sf Storage= 43 cf
Plug-Flow detention time= 54.6 min calculated for 148 cf ( $100 \%$ of inflow)
Center-of-Mass det. time $=53.7 \mathrm{~min}(810.5-756.8)$

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | :---: | :---: | :---: |
| \#1A | 44.00' | 109 cf | 6.40 'W x 14.00'L x 5.00'H Field A |
|  |  |  | 448 cf Overall - 177 cf Embedded $=271$ cf $\times 40.0 \%$ Voids |
| \#2A | 45.00' | 133 cf | Concrete Galley $4 \times 4 \times 4 \times 3$ Inside \#1 |
|  |  |  | Inside= 42.0"W x 43.0"H => $12.67 \mathrm{sf} \times 3.50 \mathrm{~L}=44.3 \mathrm{cf}$ |
|  |  | 242 cf | Total Available Storage |

Storage Group A created with Chamber Wizard

| Device | Routing | Invert | Outlet Devices |
| :---: | :--- | :---: | :--- |
| \#1 | Discarded | $44.00^{\prime}$ | $\mathbf{2 . 4 1 0}$ in/hr Exfiltration over Surface area |

Discarded OutFlow Max=0.00 cfs @ 11.55 hrs HW=44.05' (Free Discharge)
$\mathbf{L}_{1=\text { Exfiltration (Exfiltration Controls } 0.00 \mathrm{cfs} \text { ) }}$

## Summary for Subcatchment 1S: PR-1

Runoff $=$
Routed to Reach 1R: DP1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.95"

|  | Area (sf) | CN | Roofs, HSG A |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1,044 | 98 |  |  |  |
|  | 168 | 98 P | Paved parking, HSG A |  |  |
|  | 738 | $39>$ | >75\% Permeable Pavers, Good, HSG A |  |  |
|  | 188 | $39>$ | >75\% Grass cover, Good, HSG A |  |  |
|  | 2,138 | 72 | Weighted Average |  |  |
|  | 926 |  | 43.31\% Pervious Area |  |  |
|  | 1,212 |  | 56.69\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope $(\mathrm{ft} / \mathrm{ft})$ | Velocity $(\mathrm{ft} / \mathrm{sec})$ <br> (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \end{array}$ | Description |
| 6.0 |  |  |  |  | Direct Entry, Ass |

## Summary for Subcatchment 2Sa: PR-2

Runoff $=\quad 0.15$ cfs @ 12.13 hrs, Volume= 504 cf, Depth> 4.59"
Routed to Reach 2R : DP2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.95"

|  | Area (sf) | CN D | Deoscription |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1,044 | 98 R |  |  |  |
|  | 244 | 98 P | Paved parking, HSG A |  |  |
|  | 28 | $39>$ | >75\% Grass cover, Good, HSG A |  |  |
|  | 1,316 | 97 V | Weighted Average |  |  |
|  | 28 |  | 2.13\% Pervious Area |  |  |
|  | 1,288 |  | 97.87\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |

Summary for Subcatchment 2Sb: PR-2
Runoff $=0.06$ cfs @ 12.13 hrs, Volume= 224 cf, Depth> 4.71" Routed to Pond 2P : Leaching Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 10-Year Rainfall=4.95"

|  | Area (sf) | CN |
| ---: | ---: | :--- | Description $\quad$| 256 | 98 | Paved parking, HSG A |
| :--- | ---: | :--- |
| 315 | 98 | Patio, HSG A |
| 571 | 98 | Weighted Average |
| 571 |  | 100.00\% Impervious Area |


| Tc <br> $(\mathrm{min})$ | Length <br> $(\mathrm{feet})$ |
| ---: | ---: | | Slope |
| ---: |
| $(\mathrm{ft} / \mathrm{ft})$ | | Velocity |
| ---: |
| $(\mathrm{ft} / \mathrm{sec})$ | | Capacity |
| ---: |
| $(\mathrm{cfs})$ |$\quad$ Description | Direct Entry, Assumed |
| :--- |

Summary for Reach 1R: DP1


Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Reach 2R: DP2

| In | 1,316 sf, 97.87\% Impervious, | epth > 4.59" for 10-Year event |
| :---: | :---: | :---: |
| Inflow | 0.15 cfs @ 12.13 hrs , Volume= | 504 cf |
| Outflow | 0.15 cfs @ 12.13 hrs , Volume= | 504 cf, Atten= 0\%, Lag= 0.0 m |

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Pond 2P: Leaching Basin



Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev=45.78' @ 13.23 hrs Surf.Area= 90 sf Storage= 79 cf
Plug-Flow detention time= 110.4 min calculated for 224 cf ( $100 \%$ of inflow)
Center-of-Mass det. time $=109.6 \mathrm{~min}$ (858.6-749.0)

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | :---: | :---: | :---: |
| \#1A | 44.00' | 109 cf | $6.40^{\prime} \mathrm{W} \times 14.00^{\prime} \mathrm{L} \times 5.00^{\prime} \mathrm{H}$ Field A <br> 448 cf Overall -177 cf Embedded $=271$ cf $\times 40.0 \%$ Voids |
| \#2A | 45.00' | 133 cf | Concrete Galley $4 \times 4 \times 4 \times 3$ Inside \#1 Inside $=42.0^{\prime} \mathrm{W} \times 43.0 \mathrm{H} \mathrm{H}=>12.67 \mathrm{sf} \times 3.50^{\prime} \mathrm{L}=44.3 \mathrm{cf}$ Outside $=52.8^{\prime \prime} \mathrm{W} \times 48.0 \mathrm{H}=>14.72 \mathrm{sf} \times 4.00^{\prime} \mathrm{L}=58.9 \mathrm{cf}$ |
| 242 cf Total Available Storage |  |  |  |

Storage Group A created with Chamber Wizard

| Device | Routing | Invert | Outlet Devices |
| :---: | :--- | :---: | :--- |
| $\# 1$ | Discarded | $44.00^{\prime}$ | $\mathbf{2 . 4 1 0}$ in/hr Exfiltration over Surface area |

Discarded OutFlow Max=0.00 cfs @ 11.10 hrs HW=44.05' (Free Discharge)
$\mathbf{L}_{\mathbf{1}=\text { Exfiltration (Exfiltration Controls } 0.00 \mathrm{cfs} \text { ) }}$

## Summary for Subcatchment 1S: PR-1

Runoff $=\quad 0.32$ cfs @ 12.13 hrs, Volume= $\quad 943 \mathrm{cf}$, Depth> 5.29"
Routed to Reach 1R:DP1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.68"

|  | Area (sf) | CN | Roofs, HSG A |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1,044 | 98 |  |  |  |
|  | 168 | 98 P | Paved parking, HSG A |  |  |
|  | 738 | $39>$ | >75\% Permeable Pavers, Good, HSG A |  |  |
|  | 188 | $39>$ | >75\% Grass cover, Good, HSG A |  |  |
|  | 2,138 | 72 | Weighted Average |  |  |
|  | 926 |  | 43.31\% Pervious Area |  |  |
|  | 1,212 |  | 56.69\% Impervious Area |  |  |
| $\begin{array}{r} \mathrm{Tc} \\ (\mathrm{~min}) \\ \hline \end{array}$ | Length (feet) | Slope $(\mathrm{ft} / \mathrm{ft})$ | Velocity $(\mathrm{ft} / \mathrm{sec})$ <br> (ft/sec) | $\begin{array}{r} \text { Capacity } \\ \text { (cfs) } \end{array}$ | Description |
| 6.0 |  |  |  |  | Direct Entry, Ass |

## Summary for Subcatchment 2Sa: PR-2

Runoff $=\quad 0.26$ cfs @ 12.13 hrs, Volume= 912 cf, Depth> 8.31"
Routed to Reach 2R : DP2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs NRCC 24-hr C 100-Year Rainfall=8.68"


|  | Area (sf) | CN |
| ---: | ---: | :--- | Description $\quad$| 256 | 98 | Paved parking, HSG A |
| :--- | ---: | :--- |
| 315 | 98 | Patio, HSG A |
| 571 | 98 | Weighted Average |
| 571 |  | 100.00\% Impervious Area |

\(\left.$$
\begin{array}{rrrr}\begin{array}{r}\text { Tc } \\
(\mathrm{min})\end{array} & \begin{array}{r}\text { Length } \\
(\mathrm{feet})\end{array} & \begin{array}{r}\text { Slope } \\
(\mathrm{ft} / \mathrm{ft})\end{array} & \begin{array}{r}\text { Velocity } \\
(\mathrm{ft} / \mathrm{sec})\end{array}\end{array}
$$ \begin{array}{r}Capacity <br>

(\mathrm{cfs})\end{array}\right)\) Description | Direct Entry, Assumed |
| :--- |

## Summary for Reach 1R: DP1

| Inflow Area = | 2,138 | 56.69\% Impervious | 5.29" for |
| :---: | :---: | :---: | :---: |
| Inflow | 0.32 cfs @ | 12.13 hrs , Volume= | 943 cf |
| Outflow | 0.32 cfs @ | 12.13 hrs , Volume= | 943 cf, Atten= 0\%, Lag= 0.0 |

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Reach 2R: DP2

| Inflow Area $=$ | 1,316 sf, $97.87 \%$ Impervious, | Inflow Depth $>88.31 "$ | for $100-$ Year event |  |
| :--- | :--- | :--- | :--- | :--- |
| Inflow | $=$ | $0.26 \mathrm{cfs} @$ | 12.13 hrs , Volume= | 912 cf |
| Outflow | $=$ | $0.26 \mathrm{cfs} @ 12.13 \mathrm{hrs}$, Volume $=$ | 912 cf , Atten $=0 \%$, Lag $=0.0 \mathrm{~min}$ |  |

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Pond 2P: Leaching Basin



Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Peak Elev= 47.59' @ 14.29 hrs Surf.Area= 90 sf Storage= 179 cf
Plug-Flow detention time $=234.6 \mathrm{~min}$ calculated for 319 cf ( $80 \%$ of inflow)
Center-of-Mass det. time $=149.5 \mathrm{~min}(889.9-740.5$ )

| Volume | Invert | Avail.Storage | Storage Description |
| :---: | :---: | :---: | :---: |
| \#1A | 44.00' | 109 cf | 6.40 'W x 14.00'L x 5.00 'H Field A |
|  |  |  | 448 cf Overall - 177 cf Embedded $=271$ cf $\times 40.0 \%$ Voids |
| \#2A | 45.00' | 133 cf | Concrete Galley $4 \times 4 \times 4 \times 3$ Inside \#1 |
|  |  |  | Inside= 42.0"W x 43.0"H => $12.67 \mathrm{sf} \times 3.50 \mathrm{~L}=44.3 \mathrm{cf}$ |
|  |  | 242 cf | Total Available Storage |

Storage Group A created with Chamber Wizard

| Device | Routing | Invert | Outlet Devices |
| :---: | :--- | :---: | :--- |
| $\# 1$ | Discarded | $44.00^{\prime}$ | $\mathbf{2 . 4 1 0}$ in/hr Exfiltration over Surface area |

Discarded OutFlow Max=0.00 cfs @ 10.05 hrs HW=44.05' (Free Discharge)
-1=Exfiltration (Exfiltration Controls 0.00 cfs )

Stage-Area-Storage for Pond 2P: Leaching Basin

| Elevation <br> (feet) | Surface <br> (sq-ft) | Storage <br> (cubic-feet) | Elevation <br> (feet) | Surface <br> (sq-ft) | Storage <br> (cubic-feet) |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 44.00 | 90 | 0 | 46.65 | 90 | 127 |
| 44.05 | 90 | 2 | 46.70 | 90 | 130 |
| 44.10 | 90 | 4 | 46.75 | 90 | 133 |
| 44.15 | 90 | 5 | 46.80 | 90 | 136 |
| 44.20 | 90 | 7 | 46.85 | 90 | 138 |
| 44.25 | 90 | 9 | 46.90 | 90 | 141 |
| 44.30 | 90 | 11 | 46.95 | 90 | 144 |
| 44.35 | 90 | 13 | 47.00 | 90 | 147 |
| 44.40 | 90 | 14 | 47.05 | 90 | 150 |
| 44.45 | 90 | 16 | 47.10 | 90 | 152 |
| 44.50 | 90 | 18 | 47.15 | 90 | 155 |
| 44.55 | 90 | 20 | 47.20 | 90 | 158 |
| 44.60 | 90 | 22 | 47.25 | 90 | 161 |
| 44.65 | 90 | 23 | 47.30 | 90 | 163 |
| 44.70 | 90 | 25 | 47.35 | 90 | 166 |
| 44.75 | 90 | 27 | 47.40 | 90 | 169 |
| 44.80 | 90 | 29 | 47.45 | 90 | 172 |
| 44.85 | 90 | 30 | 47.50 | 90 | 174 |
| 44.90 | 90 | 32 | 47.55 | 90 | 177 |
| 44.95 | 90 | 34 | 47.60 | 90 | 180 |
| 45.00 | 90 | 36 | 47.65 | 90 | 183 |
| 45.05 | 90 | 39 | 47.70 | 90 | 185 |
| 45.10 | 90 | 41 | 47.75 | 90 | 188 |
| 45.15 | 90 | 44 | 47.80 | 90 | 191 |
| 45.20 | 90 | 47 | 47.85 | 90 | 194 |
| 45.25 | 90 | 49 | 47.90 | 90 | 196 |
| 45.30 | 90 | 52 | 47.95 | 90 | 199 |
| 45.35 | 90 | 55 | 48.00 | 90 | 202 |
| 45.40 | 90 | 58 | 48.05 | 90 | 205 |
| 45.45 | 90 | 61 | 48.10 | 90 | 207 |
| 45.50 | 90 | 63 | 48.15 | 90 | 210 |
| 45.55 | 90 | 66 | 48.20 | 90 | 213 |
| 45.60 | 90 | 99 | 48.25 | 90 | 216 |
| 45.65 | 90 | 72 | 48.30 | 90 | 218 |
| 45.70 | 90 | 75 | 48.35 | 90 | 221 |
| 45.75 | 90 | 77 | 48.40 | 90 | 224 |
| 45.80 | 90 | 80 | 48.45 | 90 | 227 |
| 45.85 | 90 | 83 | 48.50 | 90 | 229 |
| 45.90 | 90 | 86 | 48.55 | 90 | 232 |
| 45.95 | 90 | 88 | 48.60 | 90 | 234 |
| 46.00 | 90 | 91 | 48.65 | 90 | 235 |
| 46.05 | 90 | 94 | 48.70 | 90 | 236 |
| 46.10 | 90 | 97 | 48.75 | 90 | 237 |
| 46.15 | 90 | 100 | 48.80 | 90 | 238 |
| 46.20 | 90 | 102 | 48.85 | 90 | 239 |
| 46.25 | 90 | 105 | 48.90 | 90 | 240 |
| 46.30 | 90 | 108 | 48.95 | 90 | 241 |
| 46.35 | 90 | 111 | 49.00 | 90 | 242 |
| 46.40 | 90 | 113 |  |  |  |
| 46.45 | 116 |  |  |  |  |
| 46.50 | 90 | 119 |  |  |  |
| 46.55 | 125 |  |  |  |  |
| 46.60 | 90 |  |  |  |  |
|  | 90 |  |  |  |  |

## APPENDIX C NRCS Soils Report



## MAP LEGEND

| Area of Interest (AOI) |  |
| :--- | :--- |
| $\square$ | Area of Interest (AOI) |
| Soils |  |
| $\square$ | Soil Map Unit Polygons |
| $\square$ | Soil Map Unit Lines |
| $\square$ | Soil Map Unit Points |

Special Point Features
(0) Blowout

B Borrow Pit
䟿 Clay Spot
$\diamond$ Closed Depression
Gravel Pit
$\therefore$ Gravelly Spot
(8) Landfill
A. Lava Flow

Marsh or swamp
Q Mine or Quarry
(C) Miscellaneous Water

- Perennial Water
- Rock Outcrop
$\uparrow$ Saline Spot
$\therefore$ Sandy Spot
Severely Eroded Spot
- Sinkhole

3. Slide or Slip
(2) Sodic Spot

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.
Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale

Please rely on the bar scale on each map sheet for map measurements.
Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)
Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required
This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
Soil Survey Area: Plymouth County, Massachusetts Survey Area Data: Version 15, Sep 9, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 22, 2022—Jun 5, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
| :--- | :--- | ---: | ---: |
| 110E | Canton-Chatfield-Rock outcrop <br> complex, 15 to 35 percent <br> slopes, very stony |  | 1.1 |
| 635C | Canton - Urban land - Rock <br> outcrop complex, 3 to 15 <br> percent slopes | 10.2 |  |
| Totals for Area of Interest |  | $\mathbf{1 1 . 3}$ | $\mathbf{9 0 . 2 \%}$ |

## Plymouth County, Massachusetts

## 635C-Canton - Urban land - Rock outcrop complex, 3 to 15 percent slopes

Map Unit Setting

National map unit symbol: 9y4x
Elevation: 0 to 400 feet
Mean annual precipitation: 41 to 54 inches
Mean annual air temperature: 43 to 54 degrees F
Frost-free period: 145 to 240 days
Farmland classification: Not prime farmland

## Map Unit Composition

Canton and similar soils: 35 percent
Rock outcrop: 30 percent
Urban land: 25 percent
Minor components: 10 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

## Description of Canton

## Setting

Landform: Till plains, ridges, hills
Landform position (two-dimensional): Shoulder, backslope
Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Convex
Parent material: Coarse-loamy eolian deposits over sandy and gravelly supraglacial meltout till

## Typical profile

Oi-0 to 1 inches: slightly decomposed plant material
Oe - 1 to 2 inches: moderately decomposed plant material
A - 2 to 3 inches: very fine sandy loam
$E-3$ to 4 inches: very fine sandy loam
Bw1-4 to 5 inches: very fine sandy loam
Bw2 - 5 to 15 inches: very fine sandy loam
Bw3-15 to 24 inches: fine sandy loam
$B C-24$ to 28 inches: gravelly loamy sand
2C1-28 to 49 inches: gravelly coarse sand
2C2-49 to 73 inches: gravelly loamy coarse sand

## Properties and qualities

Slope: 3 to 15 percent
Depth to restrictive feature: 20 to 36 inches to strongly contrasting textural stratification
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to $5.95 \mathrm{in} / \mathrm{hr}$ )

Natural Resources

Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.4 inches)

## Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: A
Ecological site: F144AY034CT - Well Drained Till Uplands
Hydric soil rating: No

## Description of Rock Outcrop

## Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s

## Minor Components

## Gloucester

Percent of map unit: 5 percent
Landform: Hills, ground moraines
Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Side slope
Down-slope shape: Linear
Across-slope shape: Convex
Hydric soil rating: No

## Udorthents, loamy

Percent of map unit: 5 percent
Landform position (three-dimensional): Tread
Down-slope shape: Linear
Across-slope shape: Linear
Hydric soil rating: No

## Data Source Information

Soil Survey Area: Plymouth County, Massachusetts
Survey Area Data: Version 15, Sep 9, 2022

